ENHANCING ENERGY CAPTURE IN WIND TURBINES USING A HYDROSTATIC TRANSMISSION AND DYNAMIC PITCHING

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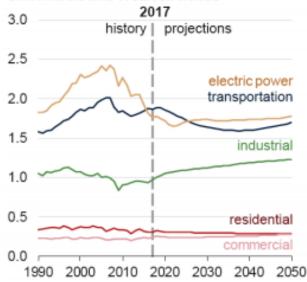




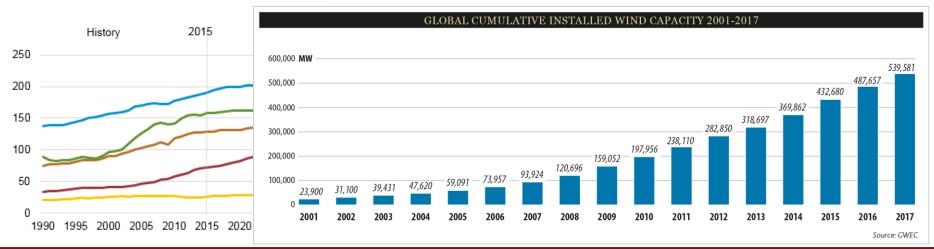


Wind statistics

Energy-related carbon dioxide emissions by sector (Reference Case) billion metric tons of carbon dioxide

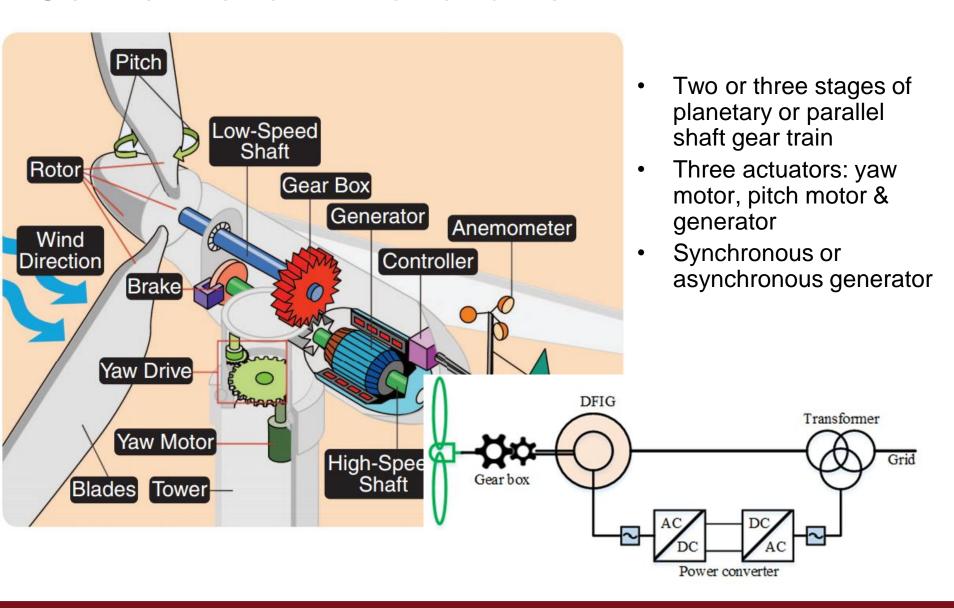


- Fastest growing new energy source
- 600 GW by 2018, 6% of the global electricity demand
- 97 GW by 2019, 7% of the U.S. electricity demand
- DOE set goal of 20% of U.S. energy from wind by 2030
- Distributed wind turbines (<1 Mw) are an attractive but under recognized means to meet this goal





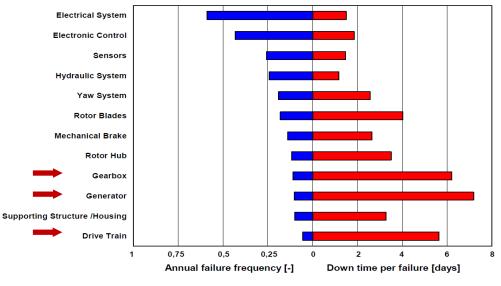
Conventional wind turbine





Conventional wind turbine





WES100 GEARBOX

Brand	Siemens (Flender)
Number of stages	2
Weight	820kg (incl. oil)
Ratio	0.0555555555556

Failure frequency and downtimes of components

Conventional drivetrain are bulky, heavy and not reliable.

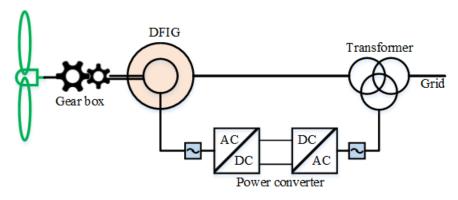


^{*} http://www.reliawind.eu/

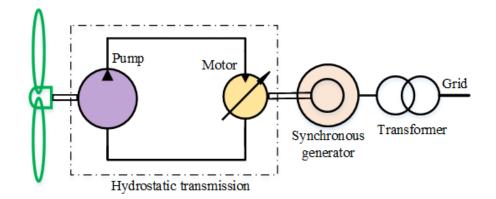




Potential of HST wind turbine



Conventional gearbox turbine



Hydrostatic wind turbine

Performance Objective

- Maximize power capture
- Minimize loads
- Reduce downtime
- Reduce maintenance cost

Hydrostatic transmission (HST)

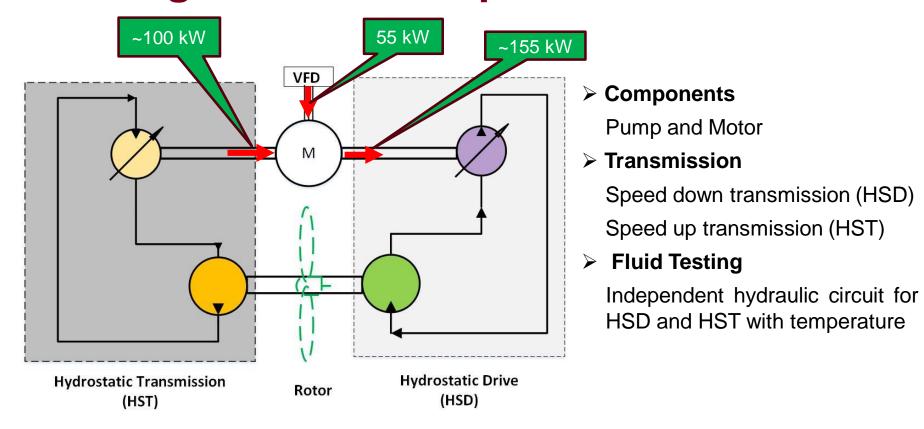
- ☐ Simple system structure
- ☐ Continuous variable transmission ratio
- No need of power converter
- ☐ All power transmitted through a fluid link;

hence less stiff

☐ Improves reliability and reduce cost



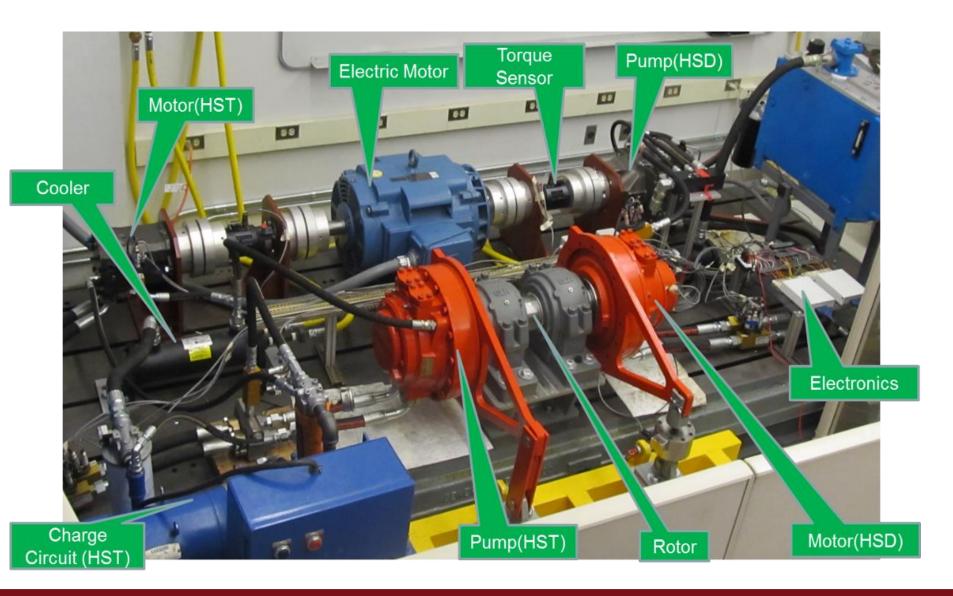
Power regenerative test platform



- > To Investigate the performance of hydrostatic transmission
- ➤ To test the advanced control algorithm
- 1. Capable of simulating a turbine output power of 100 kW
- 2. Small electric motor (55kW) to compensate for losses in the components



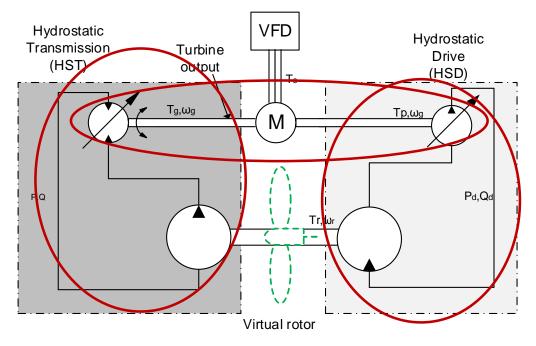
Power regenerative test platform





Dynamics of the test platform

High Speed Shaft:
$$\dot{\omega}_S = \frac{1}{J_S} \left[-b_g \omega_S + \alpha D_m P + \tau_e - \gamma D_{pd} P_d \right]$$



Input	Description	Output
$ au_e$	Variable Frequency Drive	$\omega_{\scriptscriptstyle S}$
v_d	HSD Pump Swash Voltage	P_d , ω_r , P
v	HST Motor Swash Voltage	

$\frac{\mathbf{HSD}}{\dot{P}_d} = \frac{B_d}{V_d} \left[\gamma D_{pd} \omega_s - D_{md} \omega_r - L_d P_d \right]$ $\dot{\gamma} = \frac{1}{T_d} \left[-\gamma + K_d v_d \right]$

$$\frac{\mathbf{HST}}{\dot{\omega}_r} = \frac{1}{J_r} \left[-b_r \omega_r + D_{md} P_d - D_p P \right]$$

$$\dot{P} = \frac{B}{V} \left[D_p \omega_r - \alpha D_m \omega_s - L_t P \right]$$

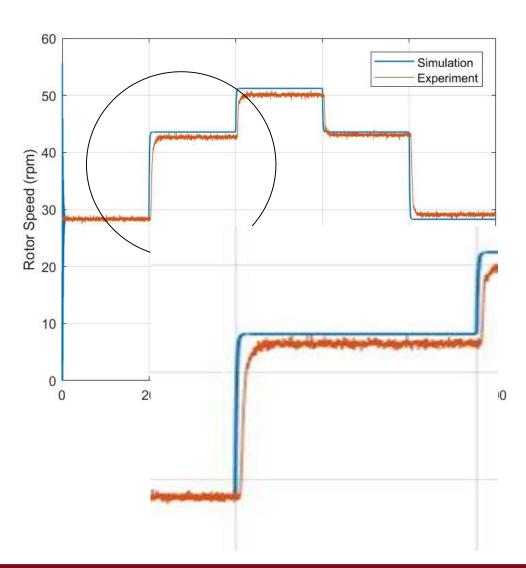
$$\dot{\alpha} = \frac{1}{T} \left[-\alpha + Kv \right]$$

Rotor Torque: $\tau_r(\omega_r, u, \beta) = D_{md}P_d\eta_{mmd}$



Experimental Validation

- > Experimental set up:
- HS Shaft Speed (ω_s):=1000 rpm
- HST Pressure (P) = 100 bar
- HSD Swash angle (α): Step of 4-6-7-6-4 volts
- At steady state, experimental results matches with simulation with maximum steady state error is 2 RPM.
- ➤ In transient case, the experimental data has slower response than the simulation.
- ➤ Because, swash plate dynamics is not included in simulation.

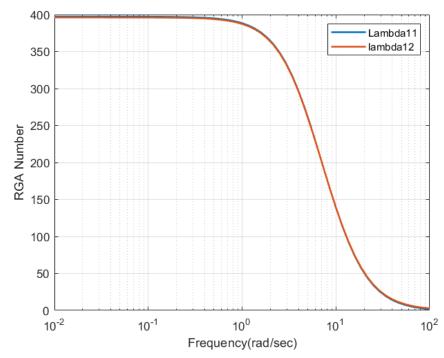




RGA Analysis

Y=[Pd P], U=[Vd V]

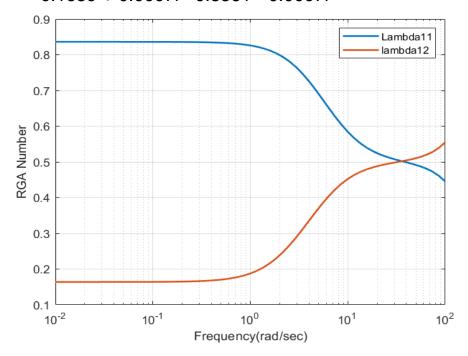
397.09 - 0.0110i -396.09 + 0.0110i -396.09 + 0.0110i 397.09 - 0.0110i



The coupling is ill conditioned

Input	Description	Output
$ au_e$	Variable Frequency Drive	ω_s
v_d	HSD Pump Swash Voltage	P_d , ω_r , P
\boldsymbol{v}	HST Motor Swash Voltage	

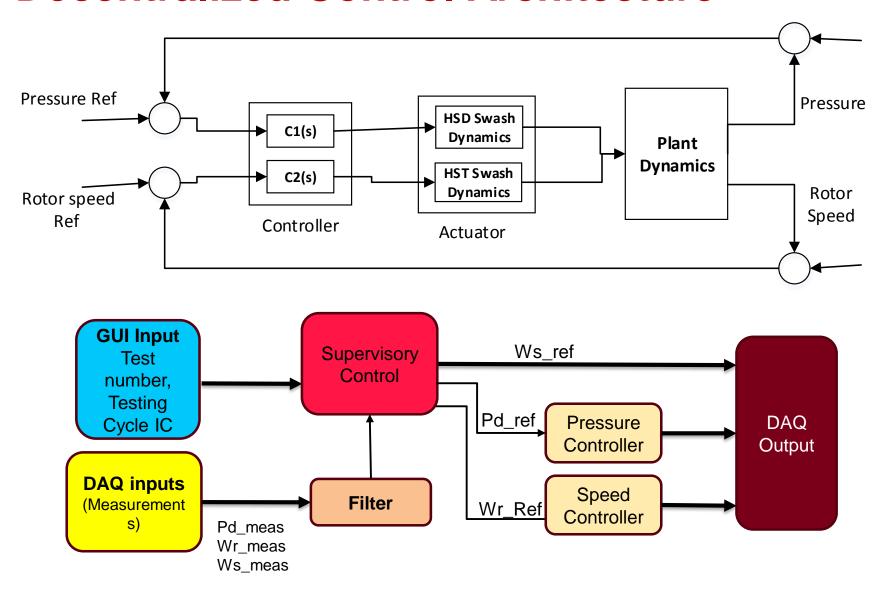
Y=[Pd Wr], U=[Vd V]



The coupling is diagonal

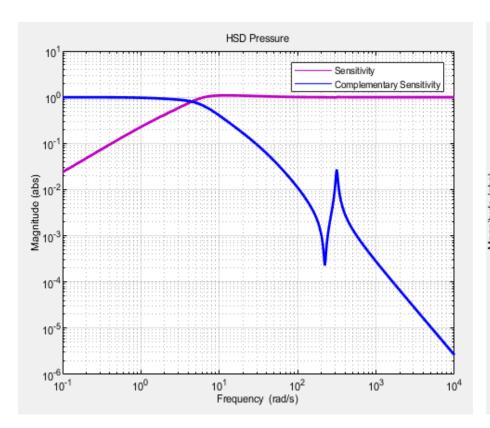


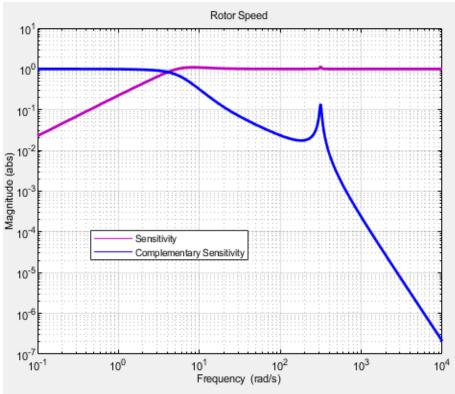
Decentralized Control Architecture





Sensitivity Analysis

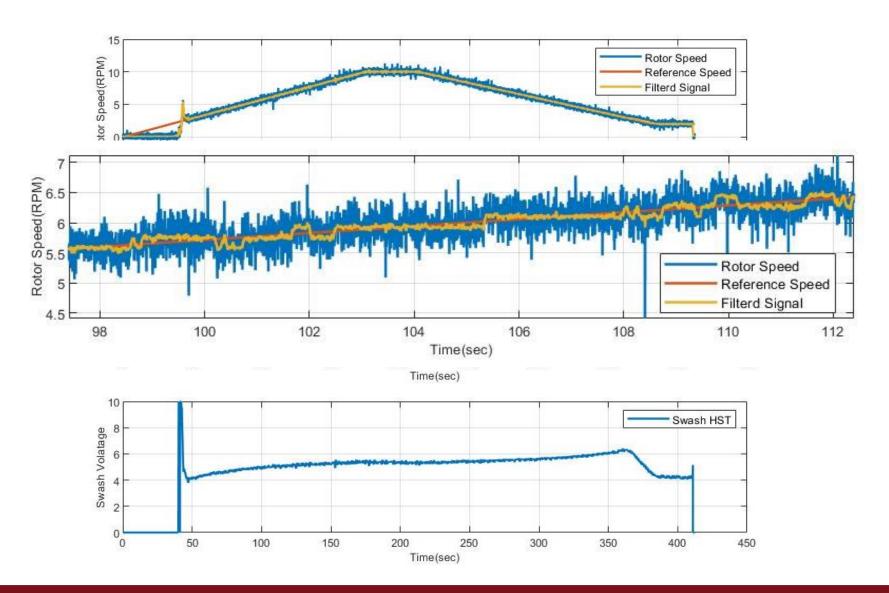




Sensitivity (S): Output/ Disturbance Compl. Sensitivity (T): Output/Reference

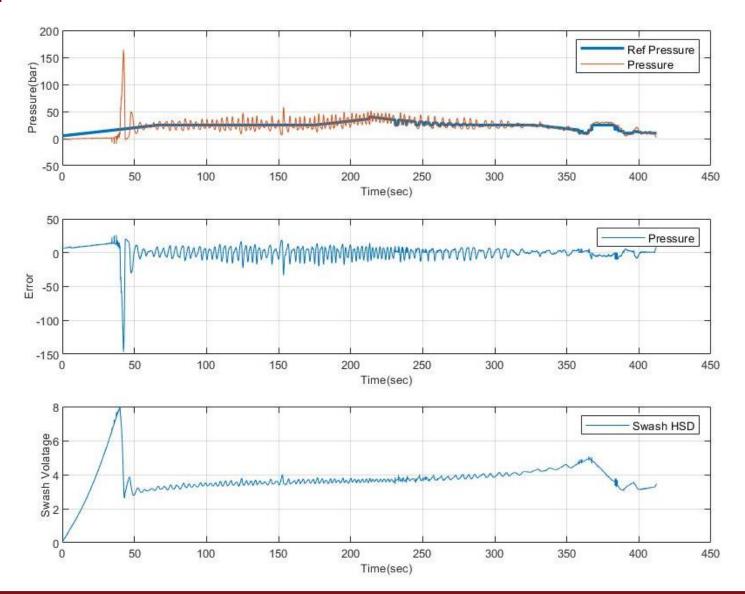


Experimental Results: Speed





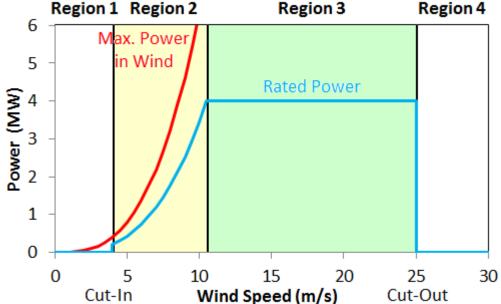
Experimental Results: Pressure





Wind Turbine Control

- Four control regions:
 - Region 1: Standby mode
 - Region 2: Control to maximize power
 - Region 3: Control to rated power
 - Region 4: Turbine shut down
- Steady wind assumed

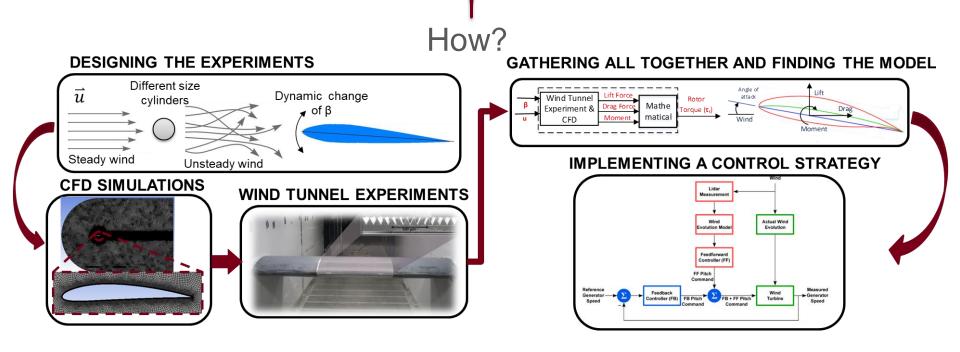


- According to Betz Law, the maximum energy that can be captured by the rotor is 59.3% of the kinetic energy of the wind
 - Best turbines nowadays harvest up to 45%
 - There is room for improvement!



Dynamic Pitching Objective

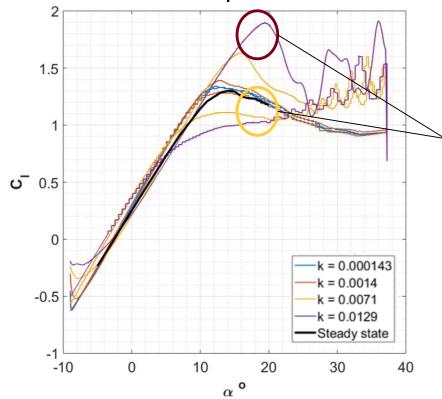
Understanding the interaction of unsteady wind and the transient response of blade pitching with the aim of improving energy capture from wind turbines

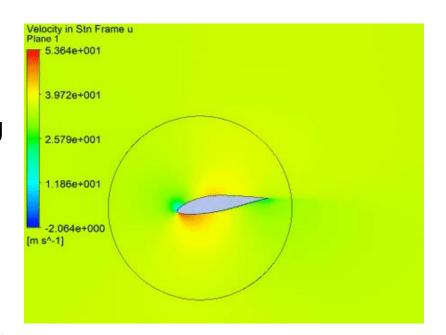




CFD Simulations

- Dynamic pitching simulations using ANSYS
- Steady state data in good correlation with published data





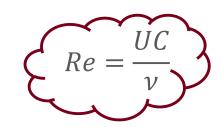
50% improvement in max lift coefficient for the dynamically pitched blade with respect to steady state

Where $k = \frac{\omega C}{2V}$ is the reduced frequency

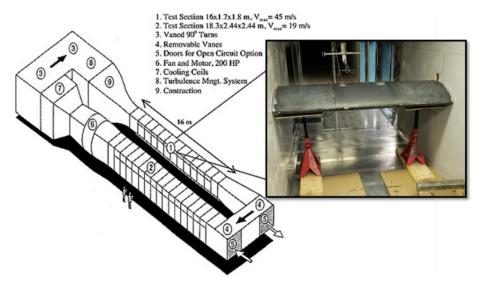
- ω rate of rotation $(\frac{rad}{s})$
- C chord length (m)
- V wind speed $(\frac{m}{s})$

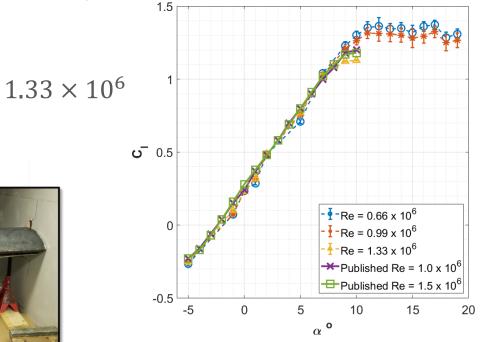


Wind Tunnel Experiments



- Recreate real-life conditions at SAFL Wind Tunnel
- Using a DU96-W-180 airfoil (commonly used in Wind Turbines)
- High Reynolds numbers (10⁶)
 - Higher wind speeds $(25\frac{m}{s})$
 - Smaller chord ($\sim 1 m$)

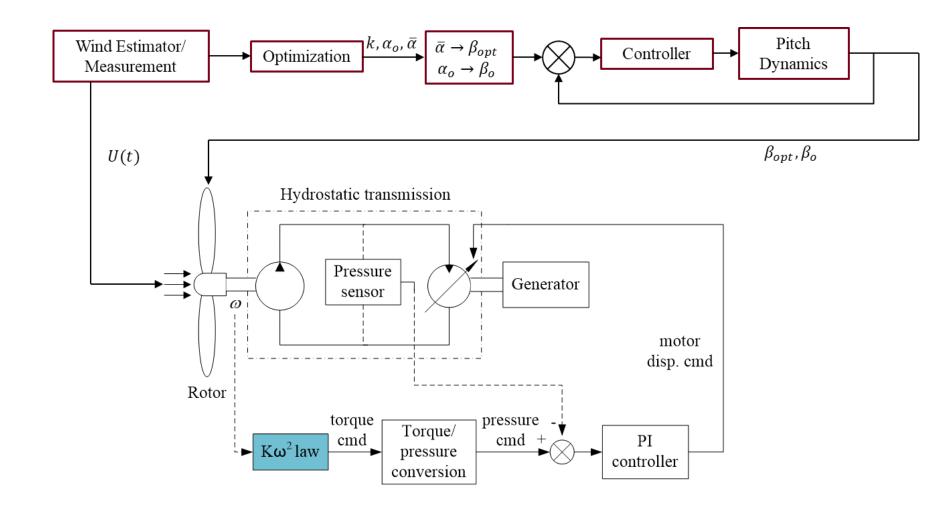




 Good correlation between experimental and published data for steady state experiments



Controls





Conclusions

- ➤ A unique power regenerative test platform has been built at the University of Minnesota to demonstrate and validate the performance of the HST. It also allows us to test different components and fluids.
- ➤ The high fidelity dynamic model closely matches the experiment data. The dynamic model will help us develop more efficient and robust controllers.
- Real time controller has been implemented on regenerative testbed.
- An HST transmission is a variable ratio, reliable, and cost effective alternative to a fixed ratio mechanical gearbox.
- Dynamics of pitch control on transient wind will be faster than the standard torque control. Faster pitch control can be achieved by using hydraulic actuators.
- Superposition of 2 controllers will improve the power capture in unsteady wind but coupling between the 2 dynamics needs to be studied





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Thank you!







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